

## Multilevel Optical Modulator Utilizing PLC-LiNbO<sub>3</sub> Hybrid-integration Technology

*Shinji Mino<sup>†</sup>, Hiroshi Yamazaki, Takashi Goh, and Takashi Yamada*

### Abstract

Multilevel optical modulators are key devices for optical transmission systems with transmission rates of 100 Gbit/s and beyond. For such modulators, NTT Photonics Laboratories has developed hybrid-integration technology for silica planar lightwave circuits (PLCs) and LiNbO<sub>3</sub> phase modulator arrays. This makes possible various kinds of multilevel modulator featuring a compact size, low loss, and high scalability. We review our recent progress in PLC-LiNbO<sub>3</sub> technology and describe some integrated multilevel modulators: 100-Gbit/s PDM-QPSK and post-100G OFDM-QPSK and 64QAM modulators (PDM: polarization-division multiplexing, QPSK: quadrature phase-shift keying, 100G: 100-Gbit/s, OFDM: orthogonal frequency-division multiplexing, QAM: quadrature amplitude modulation).

### 1. Introduction

Future large-capacity wavelength-division-multiplexing (WDM) transmission systems will require advanced spectrally efficient multilevel modulation formats, such as N-level phase-shift keying (N-PSK), N-level quadrature amplitude modulation (N-QAM), and orthogonal frequency-division multiplexing (OFDM), combined with polarization-division multiplexing (PDM) [1]. High-level QAMs have been used in the latest record-setting experiments: transmission of 69.1 Tbit/s using PDM-16QAM [2], the highest spectral efficiency (SE) for 100-Gbit/s/ch-class transmission of 9.0 bit/s/Hz with PDM-64QAM [3], and the highest potential SE of 12.4 bit/s/Hz with PDM-512QAM [4] (ch: channel). OFDM is promising not only for achieving a high SE [5], but also for enabling a bandwidth-variable optical network for efficient use of the spectral resource [6].

To accomplish those advanced modulations, multilevel electronics, such as arbitrary waveform genera-

tors or digital-to-analog converters, have been used in many transmission experiments [3], [4], [7]. They let us cover various modulation formats with a simple optical setup. On the other hand, optical multilevel-signal syntheses, in which only binary electronics are used, have also been studied extensively [2], [5], [8]–[22]. Those schemes are promising for high-speed multilevel modulations because binary electronics pose fewer challenges for high-speed operation than multilevel electronics do [13], [15], [16].

In this article, we briefly review technologies for optical multilevel-signal syntheses and describe our recent work on integrated multilevel optical modulators using a hybrid configuration of silica planar lightwave circuits (PLCs) and LiNbO<sub>3</sub> (LN) phase modulators.

### 2. Optical multilevel-signal syntheses and integrated optical modulators

There have been many studies in which multilevel optical modulations are achieved with combinations of simple commercially available modulators, such as Mach-Zehnder modulators (MZMs), straight phase

<sup>†</sup> NTT Photonics Laboratories  
Atsugi-shi, 243-0198 Japan

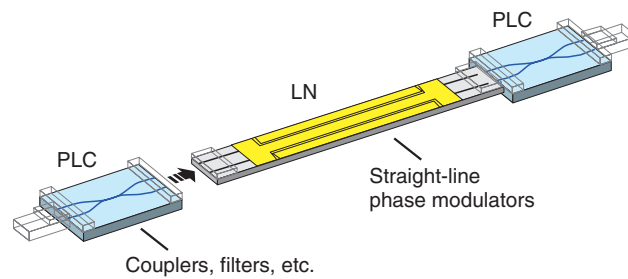


Fig. 1. PLC-LN structure.

modulators, and I/Q modulators with a dual-parallel MZM configuration (I: in-phase component, Q: quadrature component). By connecting those modulators in tandem and adjusting the amplitude of each binary driving signal to an appropriate value, researchers have achieved multilevel modulations, such as 8PSK [8], 16APSK [9], [10], 8QAM [11], and 16QAM [11], with high baud rates (ASPK: amplitude and phase key shifting).

Integrated multilevel modulators have also attracted much attention [12]–[22]. The integration provides two major advantages. First, the transmitter setup is significantly smaller. Second, we can connect modulator components in parallel much more easily than in the case of discrete modulators because integration eliminates fiber connection, which causes optical-phase fluctuation. A parallel configuration enables us to use *superposed modulation*, which was originally demonstrated with high-speed microwave transmission [23]. Integrated modulators for 16QAM have been demonstrated with several configurations, such as a quad-parallel MZM configuration fabricated with LN and PLCs [12], a five-arm configuration with quad-parallel electro-absorption modulators fabricated with InP [13], and a dual-parallel dual-tandem MZM configuration fabricated with LN [14].

In multilevel modulator design, it is worth exploiting a particular characteristic of MZMs. When the MZM is driven in a push-pull condition with a signal amplitude of  $2V\pi$  (binary PSK mode), the output optical signal has smaller distortions in symbol levels than the driving electrical signal. This is because the output optical field of the MZM varies sinusoidally with the driving voltage [15]. For various modulation formats, transmitter configurations with only  $2V\pi$  MZMs have also been investigated [15], [16]. The key to implementing those all- $2V\pi$ -MZM configurations is the integration of MZMs and high-quality passive optics because accurate control of the relative

optical amplitude and phase in each optical path is required.

To achieve such integrations with high performance levels, we have been developing hybrid integration technology for PLCs and LN phase modulators.

### 3. PLC-LN modulators

#### 3.1 Basic structure and concept

The basic structure of a hybrid-integrated PLC-LN modulator is shown in **Fig. 1**. We use an LN chip containing an array of simple straight phase modulators and PLCs containing all the other circuit components, such as couplers and filters. This structure combines the large electro-optic bandwidth of LN and the excellent transparency and design flexibility of PLCs. Another advantage is that this configuration is highly scalable because we can increase the integration level by increasing the number of phase modulator arrays in the LN chip and devising PLCs with corresponding complexity. As shown in **Fig. 2**, we have developed various modulators with increasing integration levels [17]–[22]. Each modulator circuit consists only of  $2V\pi$  MZMs and passive components. Below, we describe PLC-LN modulators based on PDM-QPSK for 100 Gbit/s and based on OFDM-QPSK and 64QAM for post-100G applications. We also briefly describe a modulator with a selectable modulation level for post-100G applications.

#### 3.2 100-Gbit/s PDM-QPSK modulator

The configuration of the PDM-QPSK modulator [19] utilizing PLC-LN integration technology is shown in **Fig. 3(a)**. Eight straight phase modulators with four high-speed signal electrodes in a Z-cut LN chip and thirteen couplers in PLCs make up two QPSK modulator circuits connected in parallel. In addition, a polarization multiplexing circuit, consisting of a polarization rotator with a half-wavelength

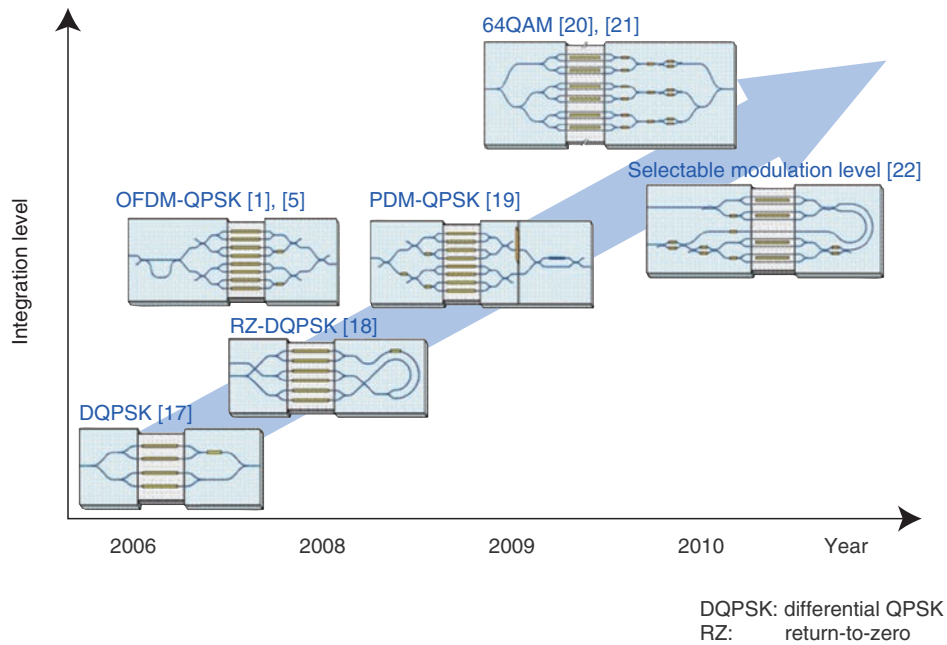


Fig. 2. PLC-LN hybrid modulators.

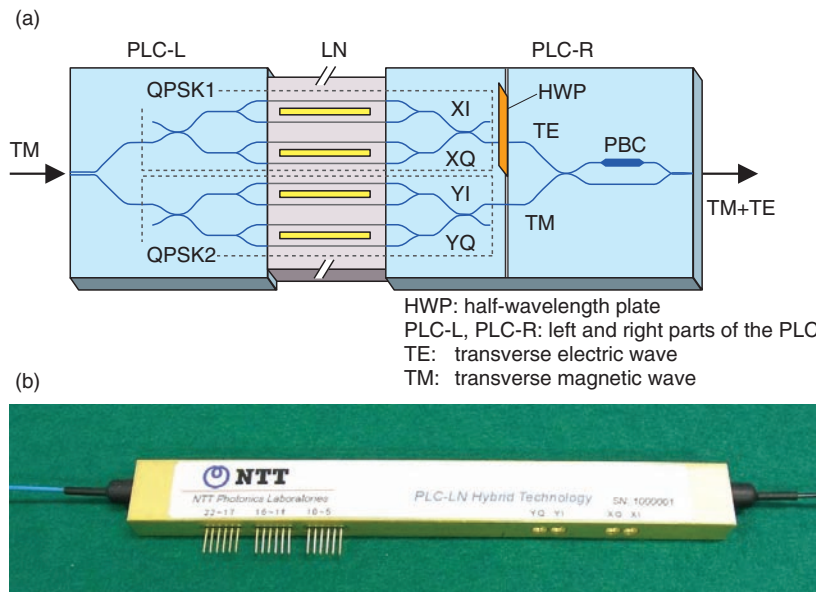


Fig. 3. (a) Configuration and (b) photograph of 100-Gbit/s PDM-QPSK utilizing PLC-LN integration technology. 100G denotes 100 Gbit/s. (package size: 118 mm x 13.5 mm x 7 mm)

plate, and a waveguide polarization beam combiner (PBC) are connected to their output. A PLC-type PBC is a compact Mach-Zehnder interferometer (MZI) about 10 mm in length and has an excellent polarization extinction ratio of greater than 25 dB over the whole C-band wavelength range [24]. A pho-

tograph of this module is shown in **Fig. 3(b)**. The module package size is 118 mm × 13.5 mm × 7 mm. Including the fiber boots on both sides, it is 131 mm long, which approaches the smallest size ever reported.

Typical characteristics of a 100-Gbit/s PDM-QPSK

modulator are listed in **Table 1**. The overall optical insertion loss of our PDM-QPSK modulator is 8.7 dB at a wavelength of 1.55  $\mu\text{m}$  including a polarization division intrinsic loss of 3 dB. The modulator's frequency response is shown in **Fig. 4**. XI, XQ, YI, and YQ correspond to the four MZMs shown in Fig. 3(a).

The modulator has an electro-optic 3-dB bandwidth of more than 27 GHz. The driving voltage was less than 3.5 V at 32 Gbit/s. The measured eye pattern for a driving voltage of 3.0 V when the modulator was driven with 32-Gbit/s non-return-to-zero  $2^{31}-1$  pseudorandom bit sequences in a back-to-back setup is shown in **Fig. 5**. Clear eye opening was obtained in this experiment. The Optical Internetworking Forum (OIF) standardized a 100-Gbit/s integrated modulator in April 2010 [25]. Our 100-Gbit/s PDM-QPSK modulator complies with the target specifications.

### 3.3 OFDM-QPSK modulator

The configuration of the OFDM-QPSK modulator [1], [5] is shown in **Fig. 6**. The modulator integrates a PLC interleave filter, two QPSK modulation circuits, each with a dual-parallel MZM configuration, and an output coupler. The input light for this modulator consists of two subcarriers, which can be generated by using another MZM driven with a clock signal. The subcarriers are separated by the interleave filter and modulated by different QPSK modulation circuits. The two QPSK signals are finally coupled and the modulator outputs a two-subcarrier OFDM-QPSK signal. The baud rate of the modulation, which is equal to the frequency spacing between the subcarriers, is 13.9 Gbaud.

The spectrum of a 111-Gbit/s PDM-OFDM-QPSK signal generated with the modulator and an external PDM circuit is shown in **Fig. 7**. The signal bandwidth is 42 GHz, which is 1.5 times the baud rate and narrow enough for 50-GHz-grid WDM transmission. Using this modulator, we achieved 13.5-Tbit/s ( $135 \times 111\text{-Gbit/s/ch}$ ) WDM transmission over a distance of 7209 km [1], [5].

### 3.4 64QAM modulator

The configuration of the 64QAM modulator [20], [21] is shown in **Fig. 8**. Three QPSK modulation circuits, each consisting of dual-parallel MZMs, are connected in parallel by a pair of PLC asymmetric  $1 \times 3/3 \times 1$  splitter/combiners, each with a power splitting/combining ratio of 4:2:1. These asymmetric circuits were designed using the wavefront-matching method, which lets us optimize the waveguide pattern

Table 1. Typical characteristics and target specifications of a 100-Gbit/s PDM-QPSK modulator.

Parameter	Achieved value	Target value
Insertion loss	8.7 dB	< 14 dB
Polarization division loss	0.1 dB	< 1.5 dB
Optical return loss	> 35 dB	> 30 dB
Extinction ratio: parent MZI child MZI	> 46 dB	> 22 dB
	> 25 dB	> 20 dB
Polarization extinction ratio	31 dB	> 20 dB
Electro-optical bandwidth	> 27 GHz	> 23 GHz
RF port $V_{\pi}$ @ 32 Gbaud	< 3.5 V	< 3.5 V

RF: radio frequency

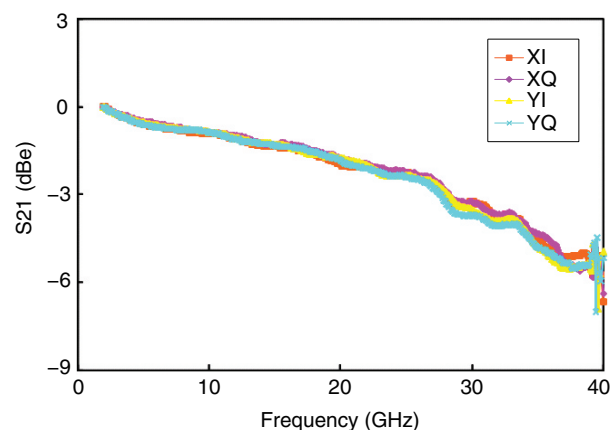


Fig. 4. Frequency response.

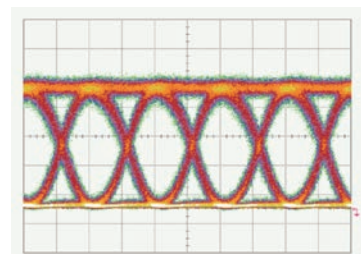


Fig. 5. Measured eye pattern.

on the basis of the desired splitting/combining ratio. PLC variable optical attenuators enable fine tuning of the power ratio. The 64QAM signal is synthesized by coupling the three QPSK signals with a field-amplitude ratio of 4:2:1 (power ratio of 16:4:1). The module has a small overall optical insertion loss of 5.5 dB,

as well as a broad electro-optic bandwidth of >25 GHz.

By driving the modulator with six 20-Gbaud binary data signals and using an external PDM circuit, we generated a 240-Gbit/s PDM-64QAM signal [20]. The signal was received with a coherent receiver using a pilotless demodulation algorithm in an offline digital signal processor. The constellations obtained with a back-to-back intradyne setup are shown in Fig. 9. The 64 signal points are clearly distinguished. The bit-error rate was better than  $1.3 \times 10^{-2}$ . Thus, we successfully demonstrated the record bit rate of 240 Gbit/s for PDM-64QAM using the modulator.

### 3.5 Selectable-modulation-level modulator

We also developed a selectable-modulation-level modulator that lets us select QPSK, 8PSK, 8QAM, or 16QAM [22], [26]. This modulator was devised for use in optical networks with a flexible modulation format, which have become the focus of attention in recent years [6]. In this modulator, we can flexibly and adaptively select a suitable multilevel modulation scheme taking account of the transmission condition.

## 4. Conclusion

We have developed PLC-LN hybrid integration technology for advanced multilevel modulators. Utilizing this technology, we have demonstrated various advanced multilevel modulators, such as a PDM-QPSK modulator for 100 Gbit/s and an OFDM-QPSK modulator, a 64QAM modulator, and a selectable-modulation-level modulator for post-100G applications. Each modulator shows excellent characteristics in terms of compact size and low insertion optical loss and a practical level of optical loss and electro-optic bandwidth. This technology is promising for optical transmission systems with channel rates of 100 Gbit/s/ch and beyond and a transfer rate well above 10 Tbit/s and for future optical networks.

## Acknowledgments

This work is partly supported by the R&D projects on “High-speed Optical Transport System Technologies” and “High-speed Optical Edge Node Technologies” of the Ministry of Internal Affairs and Communications (MIC) of Japan.

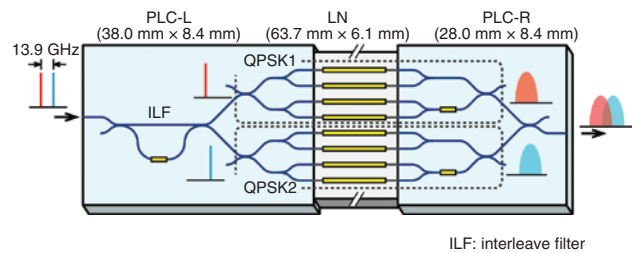


Fig. 6. Configuration of the OFDM-QPSK modulator.

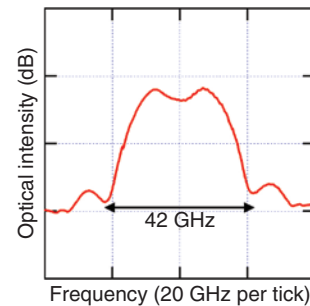


Fig. 7. Optical signal spectrum of 111-Gbit/s PDM-OFDM-QPSK signals.

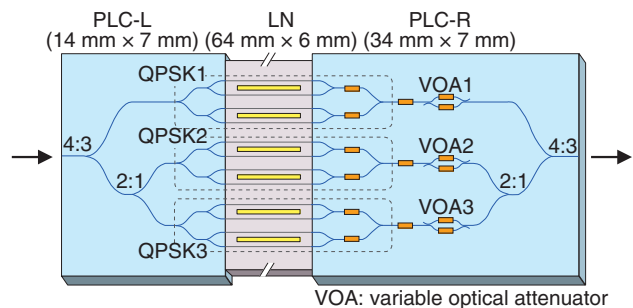


Fig. 8. Configuration of the 64QAM modulator.

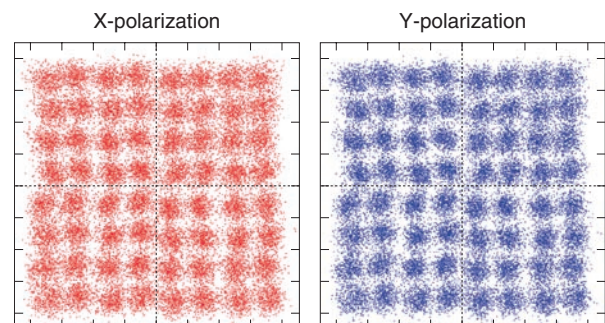


Fig. 9. Constellations of 240-Gbit/s PDM-64QAM signal.

## References

- [1] Y. Miyamoto and S. Suzuki, "Advanced Optical Modulation and Multiplexing Technologies for High-capacity OTN Based on 100 Gb/s Channel and Beyond," *IEEE Commun. Mag.*, Vol. 48, No. 3, pp. S65–S72, 2010.
- [2] A. Sano, H. Masuda, T. Kobayashi, M. Fujiwara, K. Horikoshi, E. Yoshida, Y. Miyamoto, M. Matsui, M. Mizoguchi, H. Yamazaki, Y. Sakamaki, and H. Ishii, "69.1-Tb/s (432 × 171-Gb/s) C- and Extended L-Band Transmission over 240 km Using PDM-16-QAM Modulation and Digital Coherent Detection," *Proc. of OFC/NFOEC2010*, paper PDPB7, San Diego, CA, USA.
- [3] A. Sano, T. Kobayashi, A. Matsuura, S. Yamamoto, S. Yamanaka, E. Yoshida, Y. Miyamoto, M. Matsui, M. Mizoguchi, and T. Mizuno, "100 × 120-Gb/s PDM 64-QAM Transmission over 160 km Using Linewidth-tolerant Pilotless Digital Coherent Detection," *Proc. of ECOC2010*, paper PD2.4, Torino, Italy.
- [4] S. Okamoto, K. Toyoda, T. Omiya, K. Kasai, M. Yoshida, and M. Nakazawa, "512 QAM (54 Gbit/s) Coherent Optical Transmission over 150 km with an Optical Bandwidth of 4.1 GHz," *Proc. of ECOC2010*, paper PD2.3, Torino, Italy.
- [5] H. Masuda, E. Yamazaki, A. Sano, T. Yoshimatsu, T. Kobayashi, E. Yoshida, Y. Miyamoto, S. Matsuoka, Y. Takatori, M. Mizoguchi, K. Okada, K. Hagimoto, T. Yamada, and S. Kamei, "13.5-Tb/s (135 × 111-Gb/s/ch) No-Guard-Interval Coherent OFDM Transmission over 6,248 km using SNR Maximized Second-order DRA in Extended L-band," *Proc. OFC/NFOEC'09*, paper PDPB5, San Diego, CA, USA.
- [6] H. Takara, B. Kozićki, Y. Sone, T. Tanaka, A. Watanabe, A. Hirano, K. Yonenaga, and M. Jinno, "Distance-adaptive Super-wavelength Routing in Elastic Optical Path Network (SLICE) with Optical OFDM," *Proc. of ECOC2010*, paper We.8.D.2, Torino, Italy.
- [7] S. Yamanaka, T. Kobayashi, A. Sano, H. Masuda, E. Yoshida, Y. Miyamoto, T. Nakagawa, M. Nagatani, and H. Nosaka, "11 × 171 Gb/s PDM 16-QAM Transmission over 1440 km with a Spectral Efficiency of 6.4 b/s/Hz using High-Speed DAC," *Proc. of ECOC2010*, paper We.8.C.1, Torino, Italy.
- [8] S. Tsukamoto, D. -S, Ly-Gagnon, K. Katoh, and K. Kikuchi, "Coherent Demodulation of 40-Gbit/s Polarization-multiplexed QPSK Signals with 16-GHz Spacing after 200-km Transmission," *Proc. of OFC'05*, paper OThR5, Los Angeles, CA, USA.
- [9] K. Sekine, N. Kikuchi, S. Sasaki, S. Hayase, C. Hasegawa, and T. Sugawara, "40 Gbit/s, 16-ary (4 bit/symbol) Optical Modulation/demodulation Scheme," *Electron. Lett.*, Vol. 41, No. 7, pp. 430–432, 2005.
- [10] M. Seimetz, L. Molle, M. Gruner, D. -D. Gross, and R. Freund, "Transmission Reach Attainable for Single-Polarization and PolMux Coherent Star 16QAM Systems in Comparison to 8PSK and QPSK at 10Gbaud," *Proc. OFC/NFOEC'09*, paper OTuN2, San Diego, CA, USA.
- [11] J. Yu and X. Zhou, "Ultra-high-capacity DWDM Transmission System for 100G and Beyond," *IEEE Commun. Mag.*, Vol. 48, No. 3, pp. S56–S64, 2010.
- [12] T. Sakamoto, A. Chiba, and T. Kawanishi, "50-Gb/s 16 QAM by a quad-parallel Mach-Zehnder modulator," *Proc. of ECOC2007*, paper PDS2.8, Berlin, Germany.
- [13] C. R. Doerr, P. J. Winzer, L. Zhang, L. Buhl, and N. J. Sauer, "Monolithic InP 16-QAM Modulator," *Proc. of OFC/NFOEC2008*, paper PDP20, San Diego, CA, USA.
- [14] Guo-Wei Lu, T. Sakamoto, A. Chiba, T. Kawanishi, T. Miyazaki, K. Higuma, M. Sudo, and J. Ichikawa, "16-QAM Transmitter Using Monolithically Integrated Quad Mach-Zehnder IQ Modulator," *Proc. of ECOC2010*, paper Mo.1.F.3, Torino, Italy.
- [15] N. Kikuchi, "Intersymbol Interference (ISI) Suppression Technique for Optical Binary and Multilevel Signal Generation," *J. Lightwave Technol.*, Vol. 25, No. 8, pp. 2060–2068, 2007.
- [16] T. Sakamoto, A. Chiba, and T. Kawanishi, "High-bit-rate Optical QAM," *Proc. of OFC/NFOEC'09*, paper OWG5, San Diego, CA, USA.
- [17] T. Yamada, Y. Sakamaki, T. Saida, A. Kaneko, A. Sano, and Y. Miyamoto, "86-Gbit/s Differential Quadrature Phase-shift-keying Modulator Using Hybrid Assembly Technique with Planar Lightwave Circuit and LiNbO<sub>3</sub> Devices," *Proc. of LEOS2006*, paper ThDD4, Montreal, Quebec, Canada.
- [18] T. Yamada, Y. Sakamaki, T. Shibata, A. Kaneko, A. Sano, and Y. Miyamoto, "Compact 111-Gbit/s Integrated RZ-DQPSK Modulator Using Hybrid Assembly Technique with Silica-based PLCs and LiNbO<sub>3</sub> Devices," *Proc. of OFC/NFOEC2008*, paper OThC3, San Diego, CA, USA.
- [19] H. Yamazaki, T. Yamada, K. Suzuki, T. Goh, A. Kaneko, A. Sano, E. Yamada, and Y. Miyamoto, "Integrated 100-Gb/s PDM-QPSK Modulator Using a Hybrid Assembly Technique with Silica-based PLCs and LiNbO<sub>3</sub> Phase Modulators," *Proc. of ECOC2008*, paper Mo.3.C.1, Brussels, Belgium.
- [20] A. Sano, T. Kobayashi, K. Ishihara, H. Masuda, S. Yamamoto, K. Mori, E. Yamazaki, E. Yoshida, Y. Miyamoto, T. Yamada, and H. Yamazaki, "240-Gb/s Polarization-multiplexed 64-QAM Modulation and Blind Detection Using PLC-LN Hybrid Integrated Modulator and Digital Coherent Receiver," *Proc. of ECOC2009*, paper PD2.2, Vienna, Austria.
- [21] H. Yamazaki, T. Yamada, T. Goh, Y. Sakamaki, and A. Kaneko, "64QAM Modulator with a Hybrid Configuration of Silica PLCs and LiNbO<sub>3</sub> Phase Modulators," *Photon. Technol. Lett.*, Vol. 22, No. 5, pp. 344–346, 2010.
- [22] H. Yamazaki, T. Goh, A. Mori, and S. Mino, "Modulation-level-selectable Optical Modulator with a Hybrid Configuration of Silica PLCs and LiNbO<sub>3</sub> Phase Modulators," *Proc. of ECOC2010*, paper We.8.E.1, Torino, Italy.
- [23] K. Miyauchi, S. Seki, and H. Ishio, "New Technique for Generating and Detecting Multilevel Signal Formats," *IEEE Trans. Commun.*, Vol. 24, No. 2, pp. 263–267, 1976.
- [24] T. Mizuno, T. Goh, T. Ohyama, Y. Hashizume, and A. Kaneko, "Integrated In-band OSNR Monitor Based on Planar Lightwave Circuit," *Proc. of ECOC2009*, paper 7.2.5, Vienna, Austria.
- [25] Optical Internetworking Forum (OIF): <http://www.oiforum.com/public/documents/OIF-PMQ-TX-01.0.pdf>.
- [26] H. Yamazaki and T. Goh, "Flexible-format Optical Modulators with a Hybrid Configuration of Silica Planar Lightwave Circuits and LiNbO<sub>3</sub> Phase Modulators," *NTT Technical Review*, Vol. 9, No. 4, 2011 (to be published).



**Shinji Mino**

Senior Research Engineer, Supervisor, Photonics Integration Laboratory, NTT Photonics Laboratories.

He received the B.Sc. degree in chemistry from Waseda University, Tokyo, in 1986 and the M.Sc. degree in chemistry and Ph.D. degree in electronic engineering from the University of Tokyo in 1988 and 1996, respectively. He joined NTT Opto-Electronics Laboratories (now NTT Photonics Laboratories) in 1988. From 1993, he was engaged in research on the hybrid integration of various active optical devices and electronic ICs, focusing particularly on the use of high-frequency circuits in silica PLCs. His research interests include various types of PLC hybrid integration for optical active devices and electronic ICs, such as liquid crystal devices, LiNbO<sub>3</sub> modulators, and optical semiconductor devices, such as photodiodes and laser diodes. He is a senior member of IEEE LEOS and the Institute of Electronics, Information and Communication Engineers (IEICE), and a member of the Japan Society of Applied Physics (JSAP).



**Hiroshi Yamazaki**

Research Engineer, Photonics Integration Laboratory, NTT Photonics Laboratories.

He received the B.S. degree in integrated human studies and M.S. degree in human and environmental studies from Kyoto University in 2003 and 2005, respectively. In 2005, he joined NTT Photonics Laboratories, where he engaged in research on optical waveguide devices for communication systems. His current research interests include devices and systems for optical transmission using advanced multilevel modulation formats. He is a member of IEICE.



**Takashi Goh**

Senior Research Engineer, Photonics Integration Laboratory, NTT Photonics Laboratories.

He received the B.S. and M.S. degrees in electronic and communication engineering from Waseda University, Tokyo, in 1991 and 1993, respectively. In 1993, he joined the NTT Opto-electronics Laboratories (now Photonics Laboratories), where he engaged in research on silica-based PLCs including thermo-optic switches, arrayed-waveguide grating multiplexers, multi-degree reconfigurable add-drop multiplexers, and advanced modulators. From 2002 to 2004, he was engaged in photonic network development such as ROADM ring systems in NTT Innovation Laboratories. He is a member of IEICE and JSAP.



**Takashi Yamada**

Senior Research Engineer, Photonics Integration Laboratory, NTT Photonics Laboratories.

He received the B.E. and M.E. degrees from Tohoku University, Miyagi, in 1994 and 1996, respectively. In 1996, he joined NTT Opto-electronics Laboratories (now Photonics Laboratories). Since 2001, he has been engaged in research on high-speed optical functional modulators using a hybrid-assembly technique for silica-based PLCs and LN phase modulators. He is a member of IEICE.